Chapter 9: Moments of Inertia

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Introduction

- Previously considered distributed forces which were proportional to the area or volume over which they act.
 - The resultant was obtained by summing or integrating over the areas or volumes.
 - The moment of the resultant about any axis was determined by computing the first moments of the areas or volumes about that axis.
- Will now consider forces which are proportional to the area or volume over which they act but also vary linearly with distance from a given axis.
 - It will be shown that the magnitude of the resultant depends on the first moment of the force distribution with respect to the axis.
 - The point of application of the resultant depends on the second moment of the distribution with respect to the axis.
- Current chapter will present methods for computing the moments and products of inertia for areas and masses.

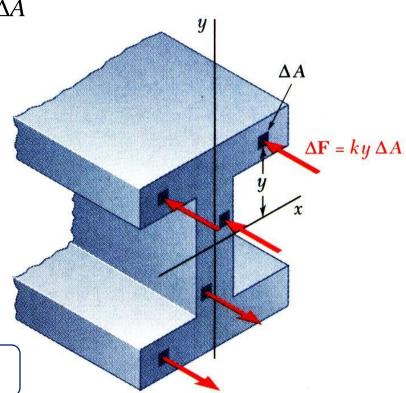
Moment of Inertia of an Area

- Consider distributed forces $\Delta \vec{F}$ whose magnitudes are proportional to the elemental areas ΔA on which they act and also vary linearly with the distance of ΔA from a given axis.
- Example: Consider a beam subjected to pure bending. Internal forces vary linearly with distance from the neutral axis which passes through the section centroid.

$$\Delta \vec{F} = ky \Delta A \quad \Longrightarrow \quad$$

 $R = \int \Delta F = k \int y \, dA = 0$ $\int y \, dA = Q_x = \text{first moment}$

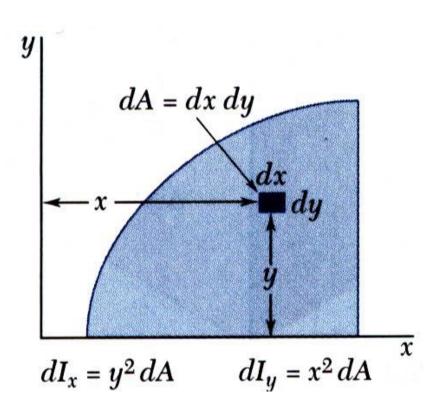
 $M = \int \Delta F \cdot y = k \int y^2 dA$ $\int y^2 dA =$ second moment



Moment of Inertia of an Area by Integration

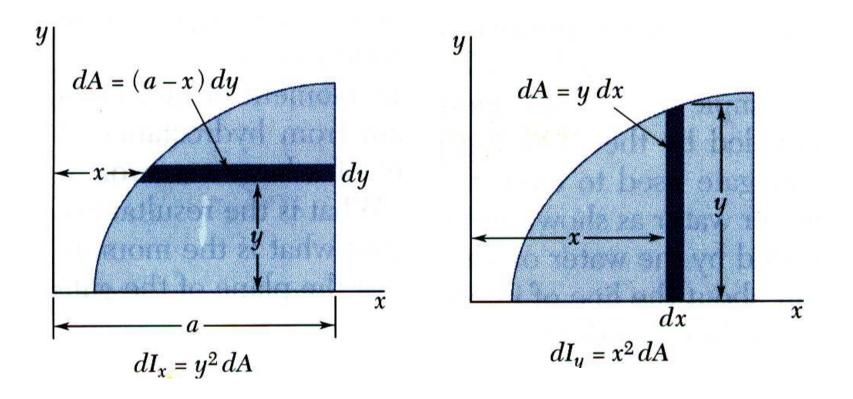
• Second moments or moments of inertia of an area with respect to the *x* and *y* axes,

$$I_x = \int y^2 dA$$
 , $I_y = \int x^2 dA$



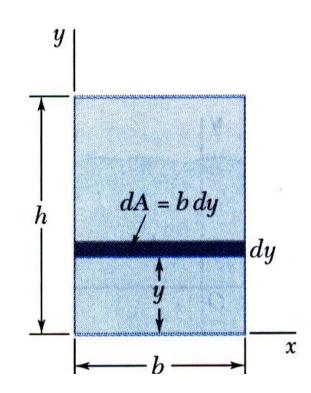
□ Moment of Inertia of an Area by Integration

• Evaluation of the integrals is simplified by choosing *dA* to be a thin strip parallel to one of the coordinate axes.



Moment of Inertia of an Area by Integration

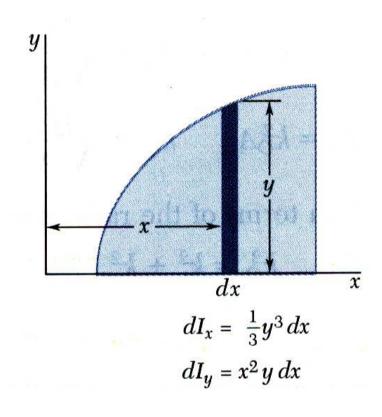
• For a rectangular area,



Moment of Inertia of an Area by Integration

• The formula for rectangular areas may also be applied to strips parallel to the axes,

$$dI_x = \frac{1}{3}y^3 dx \qquad dI_y = x^2 dA = x^2 y dx$$



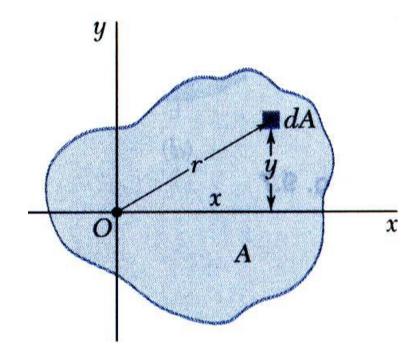
D Polar Moment of Inertia

• The *polar moment of inertia* is an important parameter in problems involving torsion of cylindrical shafts and rotations of slabs.

$$\left(J_0 = \int r^2 dA\right)$$

• The polar moment of inertia is related to the rectangular moments of inertia,

$$J_0 = \int r^2 dA = \int (x^2 + y^2) dA = \int x^2 dA + \int y^2 dA$$



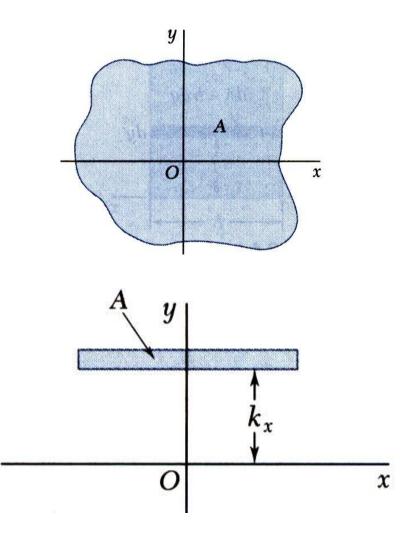
$$\Rightarrow \left(J_0 = I_y + I_x \right)$$

Radius of Gyration of an Area

• Consider area A with moment of inertia I_x . Imagine that the area is concentrated in a thin strip parallel to the x axis with equivalent I_x .

$$\begin{bmatrix} I_x = k_x^2 A \implies k_x = \sqrt{\frac{I_x}{A}} \end{bmatrix}$$

 $k_x = radius of gyration$ with respect to the x axis

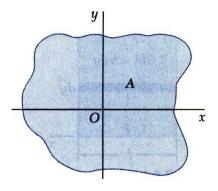


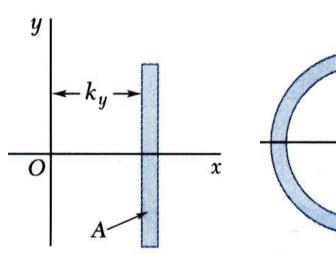
Radius of Gyration of an Area

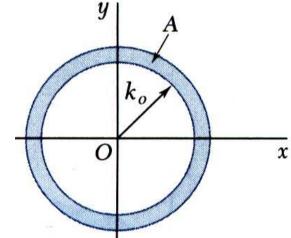
• Similarly,

$$I_{y} = k_{y}^{2}A \implies k_{y} = \sqrt{\frac{I_{y}}{A}}$$

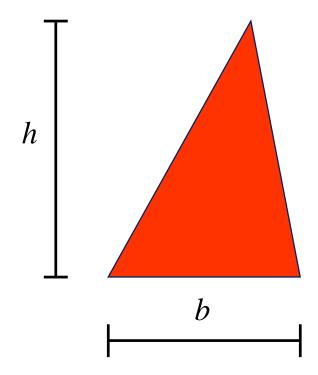
$$\left(k_O^2 = k_x^2 + k_y^2\right)$$

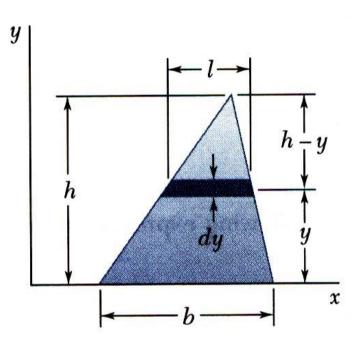




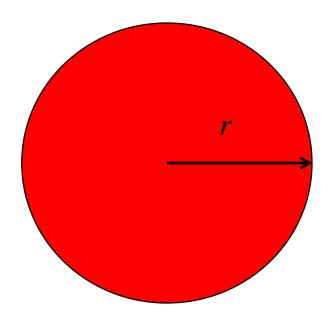


Determine the moment of inertia of a triangle with respect to its base.



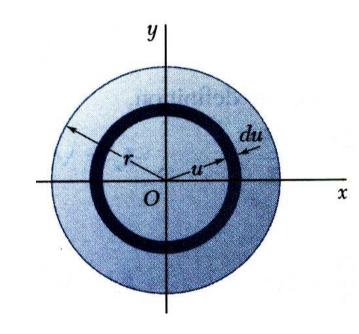


- a) Determine the centroidal polar moment of inertia of a circular area by direct integration.
- b) Using the result of part *a*, determine the moment of inertia of a circular area with respect to a diameter.

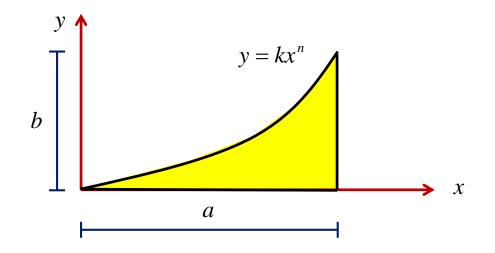


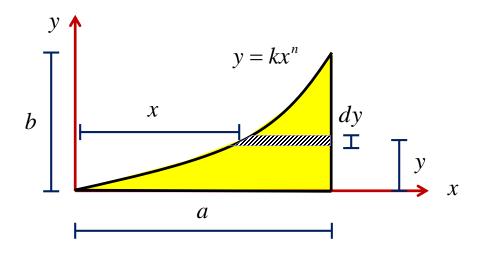
SOLUTION:

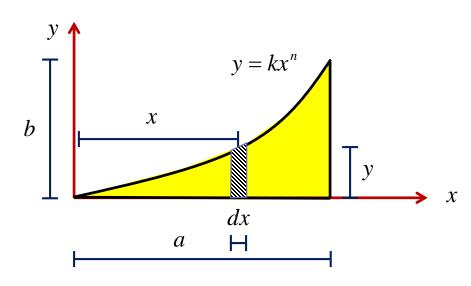
• An annular differential area element is chosen,

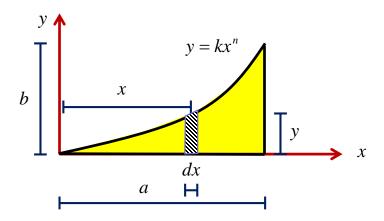


- (a) Determine the moment of inertia of the shaded area shown with respect to each of the coordinate axe.
- (b) Using the results of part a, determine the radius of gyration of the shaded area with respect to each of the coordinate axes.





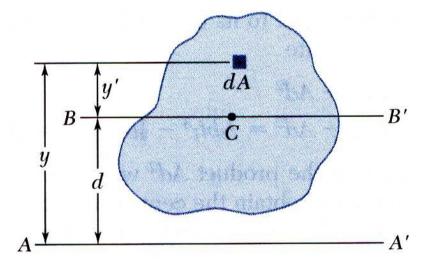




Parallel Axis Theorem

• Consider moment of inertia *I* of an area *A* with respect to the axis *AA*'

$$I = \int y^2 dA$$



• The axis *BB*' passes through the area centroid and is called a *centroidal axis*.

$$I = \int y^2 dA = \int (y'+d)^2 dA = \int y'^2 dA + 2d \int y' dA + d^2 \int dA \quad \Rightarrow \qquad \left[I = \overline{I} + Ad^2 \right]$$

parallel axis theorem

Parallel Axis Theorem

• Moment of inertia I_T of a circular area with respect to a tangent to the circle,

$$I_T = \bar{I} + Ad^2 = \frac{1}{4}\pi r^4 + (\pi r^2) r^2 \implies \left(I_T = \frac{5}{4}\pi r^4 \right)$$

$$C$$

$$d = r$$

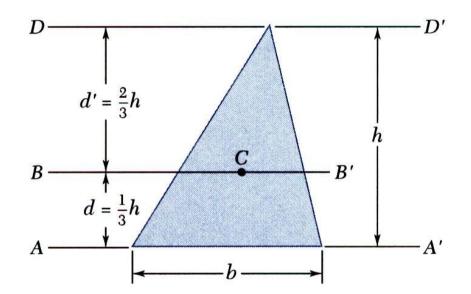
$$T$$

• Moment of inertia of a triangle with respect to a centroidal axis,

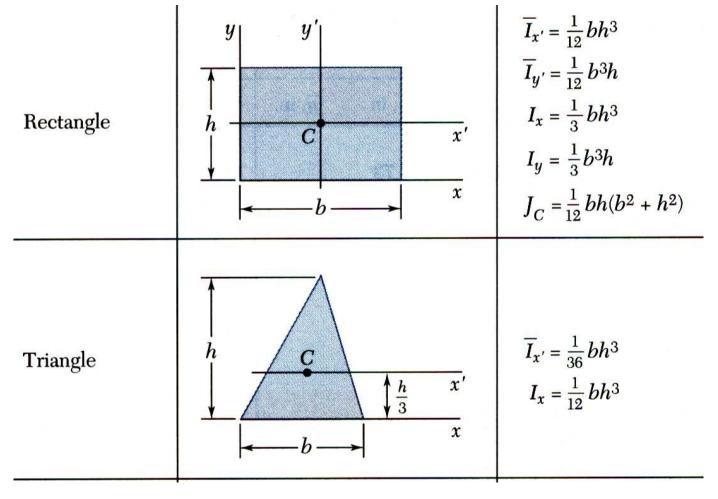
$$I_{AA'} = \bar{I}_{BB'} + Ad^2 \implies$$

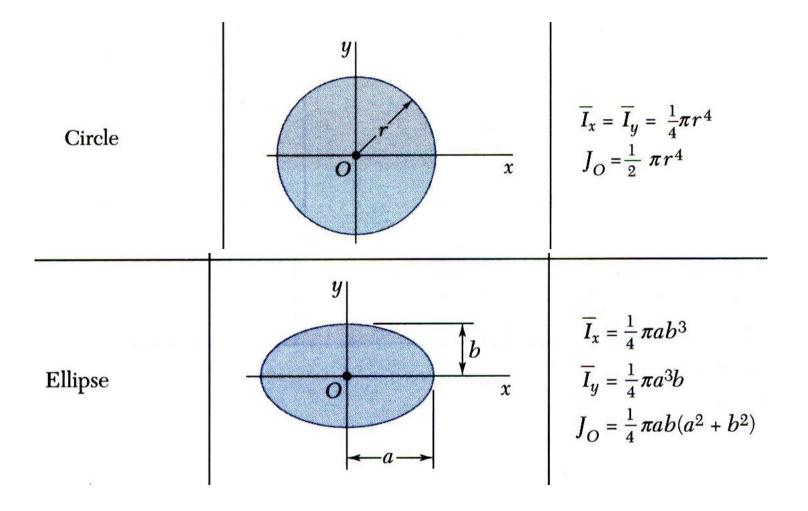
$$I_{BB'} = I_{AA'} - Ad^2 = \frac{1}{12}bh^3 - \frac{1}{2}bh\left(\frac{1}{3}h\right)^2$$

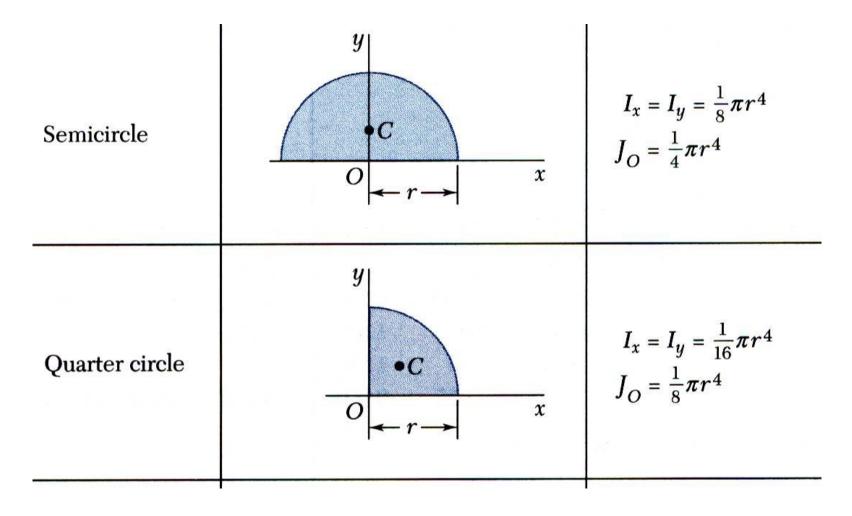
$$\implies I_{BB'} = \frac{1}{36}bh^3$$



• The moment of inertia of a composite area A about a given axis is obtained by adding the moments of inertia of the component areas A_1, A_2, A_3, \ldots , with respect to the same axis.





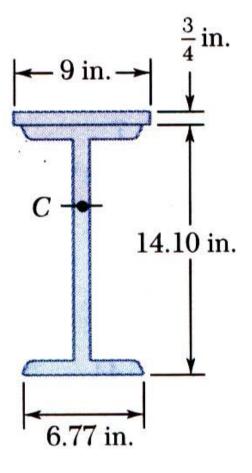


						Axis X-X		Axis Y-Y		
erret fen medriken om og et forstere	and and stars a literation of	Designation	Area mm ²	Depth mm	Width mm	$\frac{\overline{I}_x}{10^6 \text{ mm}^4}$	$ar{k_x} ar{y}$ mm mm	$\frac{\overline{I}_y}{10^6 \text{ mm}^4}$	\overline{k}_y mm	x mm
W Shapes (Wide-Flange Shapes)	Y X X Y X Y Y	$W460 \times 113^{\dagger}$ $W410 \times 85$ $W360 \times 57$ $W200 \times 46.1$	14400 10800 7230 5890	463 417 358 203	280 181 172 203	554 316 160.2 45.8	196.3 170.7 149.4 88.1	63.3 17.94 11.11 15.44	66.3 40.6 39.4 51.3	
S Shapes (American Standard Shapes)	$x \rightarrow x$	$$460 \times 81.4$$ $$310 \times 47.3$ $$250 \times 37.8$ $$150 \times 18.6$	10390 6032 4806 2362	457 305 254 152	152 127 118 84	335 90.7 51.6 9.2	179.6 122.7 103.4 62.2	8.66 3.90 2.83 0.758	29.0 25.4 24.2 17.91	
C Shapes (American Standard Channels)	$x \xrightarrow{Y} x$	$C310 \times 30.8^{\dagger}$ $C250 \times 22.8$ $C200 \times 17.1$ $C150 \times 12.2$	3929 2897 2181 1548	305 254 203 152	74 65 57 48	53.7 28.1 13.57 5.45	$ 117.1 \\ 98.3 \\ 79.0 \\ 59.4 $	$1.615 \\ 0.949 \\ 0.549 \\ 0.288$	20.29 18.11 15.88 13.64	17.73 16.10 14.50 13.00

The strength of a W14x38 rolled steel beam is increased by attaching a plate to its upper flange.

Determine the moment of inertia and radius of gyration with respect to an axis which is parallel to the plate and passes through the centroid of the section.

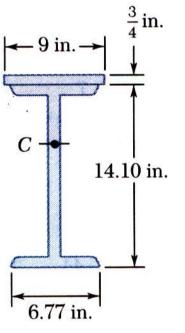
W14×38:
A = 11.20 (in²)
$$\bar{I}_x = 385$$
 (in⁴)



Section $| \Lambda(in^2) | \overline{u}(in) \rangle$

SOLUTION:

• Determine location of **the centroid of composite section** with respect to a coordinate system with **origin at the centroid of the beam section.**



$$\frac{36\text{ction}}{\text{Plate}} = \frac{N(\text{in}^{-})}{9 \times \frac{3}{4}} = 6.75 \qquad \frac{14.10}{2} + \frac{1}{2} \times \frac{3}{4} = 7.425 \qquad 50.12 \qquad \qquad 6.77 \text{ in.} \qquad \qquad 0 \qquad \qquad$$

 $|\overline{u} \Lambda (in^3)$

SOLUTION:

• Apply the parallel axis theorem to determine moments of inertia of beam section and plate with respect to composite section centroidal axis.

$$I_{x',\text{beam}} = \bar{I}_x + A\bar{Y}^2 = 385 + (11.20)(2.792)^2$$

$$\Rightarrow I_{x',\text{beam}} = 472.3 \text{ (in}^4)$$

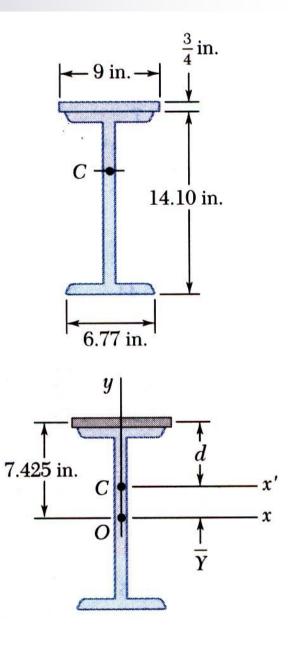
$$I_{x',\text{plate}} = \bar{I}_x + Ad^2 = \frac{1}{12}(9)\left(\frac{3}{4}\right)^3 + (6.75)(7.425 - 2.792)^2$$

$$\Rightarrow I_{x',\text{plate}} = 145.2 \text{ (in}^4)$$

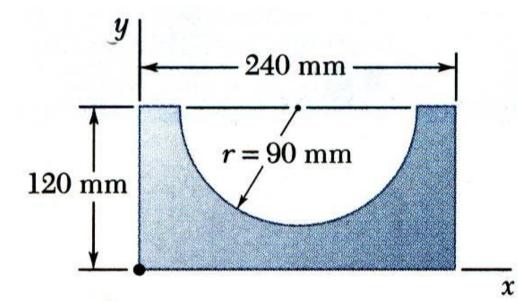
$$I_{x'} = I_{x',\text{beam}} + I_{x',\text{plate}} = 472.3 + 145.2 \implies (I_{x'} = 617.5 \,(\text{in}^4))$$

• Calculate the radius of gyration from the moment of inertia of the composite section.

$$k_{x'} = \sqrt{\frac{I_{x'}}{A}} = \sqrt{\frac{617.5 \,(\text{in}^4)}{17.95 \,(\text{in}^2)}} \quad \Rightarrow \boxed{k_{x'} = 5.87 \,(\text{in.})}$$

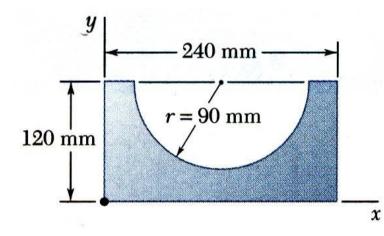


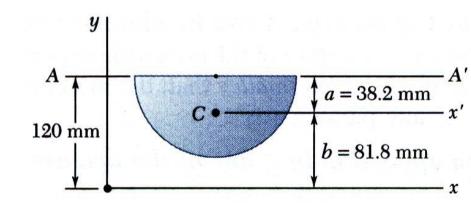
Determine the moment of inertia of the shaded area with respect to the x axis.



SOLUTION:

• Compute the moments of inertia of the bounding rectangle and half-circle with respect to the *x* axis.



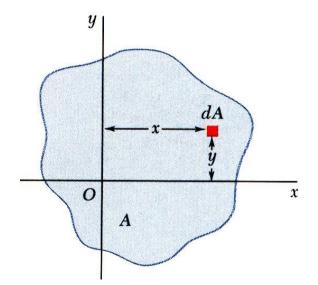


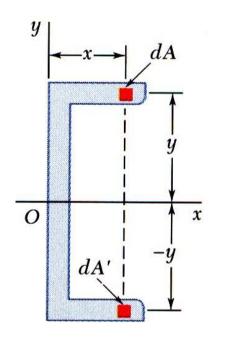
Product of Inertia

• Product of Inertia:

$$I_{xy} = \int xy \, dA$$

Unlike the moments of inertia Ix and Iy the product of inertia Ixy can be positive, negative, or zero.

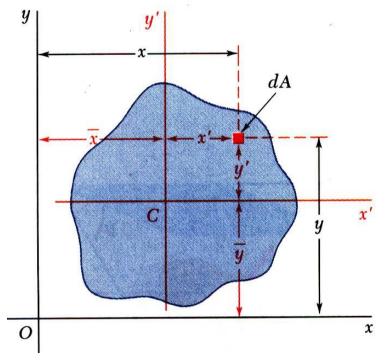




• When the *x* axis, the *y* axis, or both are an axis of symmetry, the product of inertia is zero.

Product of Inertia

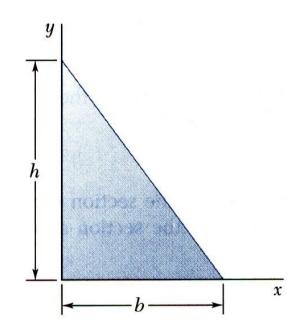
• Parallel axis theorem for products of inertia:



Determine the product of inertia of the right triangle

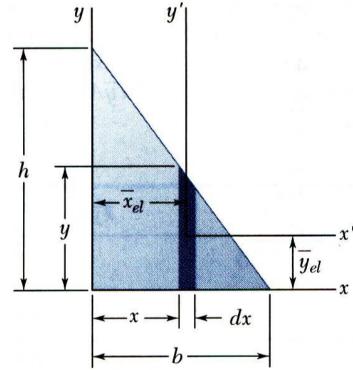
(a) with respect to the x and y axes and

(*b*) with respect to centroidal axes parallel to the *x* and *y* axes.



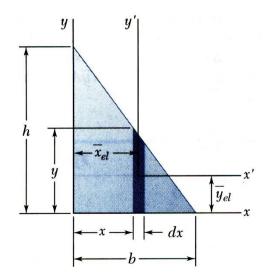
SOLUTION:

• Determine the product of inertia using direct integration with the parallel axis theorem on vertical differential area strips



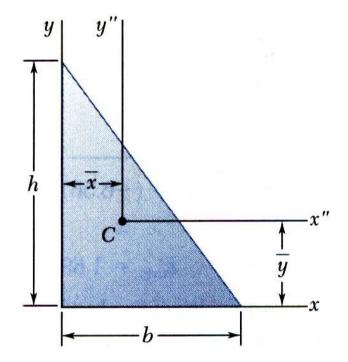
SOLUTION:

Integrating dI_x from x = 0 to x = b,

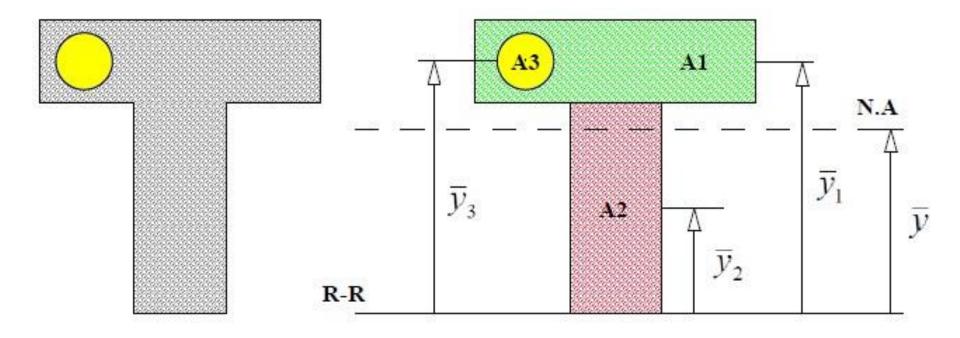


SOLUTION:

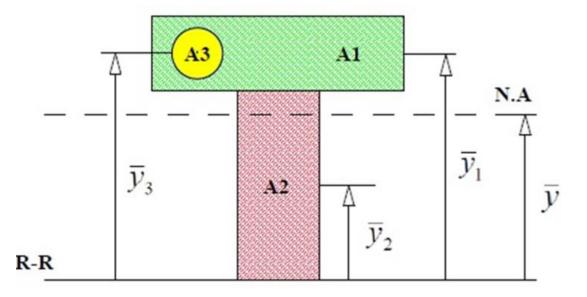
• Apply the parallel axis theorem to evaluate the product of inertia with respect to the centroidal axes.



Systematic Calculation of the Moment of Inertia



Systematic Calculation of the Moment of Inertia



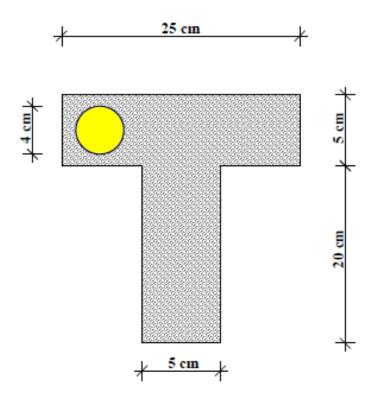
Parts	A_i	\overline{y}_i	$A_i \overline{y}_i$	$A_i \overline{y}_i^2$	I _{gi}
1	A_1	\overline{y}_1	$A_1\overline{y}_1$	$A_1 \overline{y}_1^2$	I_{g_1}
2	A_2	\overline{y}_2	$A_2 \overline{y}_2$	$A_2 \overline{y}_2^2$	I_{g_2}
3	$-A_3$	\overline{y}_3	$-A_3\overline{y}_3$	$-A_3\overline{y}_3^2$	$-I_{g_3}$
	$\sum A_i$		$\sum A_i \overline{y}_i$	$\sum A_i \overline{y}_i^2$	$\sum I_{g_i}$

Generation Systematic Calculation of the Moment of Inertia

Parts	A_i	\overline{y}_i	$A_i \overline{y}_i$	$A_i \overline{y}_i^2$	I _{gi}
1	A_1	\overline{y}_1	$A_1\overline{y}_1$	$A_1 \overline{y}_1^2$	I_{g_1}
2	A_2	\overline{y}_2	$A_2 \overline{y}_2$	$A_2 \overline{y}_2^2$	I_{g_2}
3	$-A_3$	\overline{y}_3	$-A_3\overline{y}_3$	$-A_3\overline{y}_3^2$	$-I_{g_3}$
	$\sum A_i$		$\sum A_i \overline{y}_i$	$\sum A_i \overline{y}_i^2$	$\sum I_{g_i}$

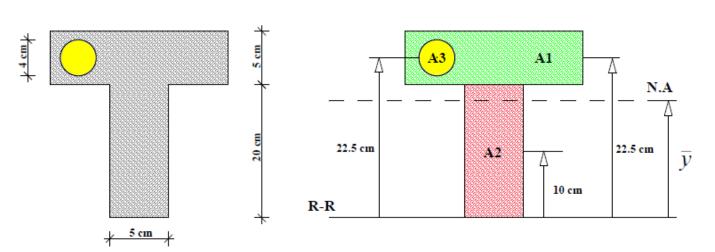
$$A = \sum A_i \qquad I_{R-R} = \sum I_{g_i} + \sum A_i \overline{y}_i^2$$
$$\overline{y} = \frac{\sum A_i \overline{y}_i}{\sum A_i} \qquad I_{NA} = \sum I_{g_i} + \sum A_i \overline{y}_i^2 - \frac{(\sum A_i \overline{y}_i)^2}{\sum A_i}$$

Determine the moment of Inertia.



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SOLUTION:



×

Parts	A_i	\overline{y}_i	$A_i \overline{y}_i$	$A_i \overline{y}_i^2$	I_{g_i}
1	$5 \times 25 = 125$	22.5	2812.5	63281.25	$\frac{1}{12}(25)(5)^3 = 260.42$
2	$5 \times 20 = 100$	10	1000	10000	$\frac{1}{12}(5)(20)^3 = 3333.33$
3	$-\pi \left(\frac{4}{2}\right)^2 = -12.57$	22.5	-282.83	- 6363.68	$-\pi \left(\frac{4}{2}\right)^4 = -50.27$
	212.43		3529.67	66917.57	3543.48

SOLUTION:

Parts	A_i	\overline{y}_i	$A_i \overline{y}_i$	$A_i \overline{y}_i^2$	I_{g_i}
1	$5 \times 25 = 125$	22.5	2812.5	63281.25	$\frac{1}{12}(25)(5)^3 = 260.42$
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3	$-\pi \left(\frac{4}{2}\right)^2 = -12.57$	22.5	-282.83	-6363.68	$-\pi \left(\frac{4}{2}\right)^4 = -50.27$
	212.43		3529.67	66917.57	3543.48

$$A = \sum A_i = 212.43 \ cm^2 \qquad \overline{y} = \frac{\sum A_i \overline{y}_i}{\sum A_i} = \frac{3529.67}{212.43} = 16.62 \ cm^2$$

$$I_{R-R} = \sum I_{g_i} + \sum A_i \bar{y}_i^2 = 3543.48 + 66917.57 = 70461.05 \ cm^4$$
$$I_{NA} = \sum I_{g_i} + \sum A_i \bar{y}_i^2 - \frac{(\sum A_i \bar{y}_i)^2}{\sum A_i} = 3543.48 + 66917.57 - \frac{(3529.67)^2}{212.43} = 11813.16 \ cm^4$$

Given:

$$I_x = \int y^2 dA$$
 , $I_y = \int x^2 dA$, $I_{xy} = \int xy dA$

we wish to determine moments and product of inertia with respect to new axes x' and y'.

Note:
$$\begin{aligned} x' &= x\cos\theta + y\sin\theta\\ y' &= y\cos\theta - x\sin\theta \end{aligned}$$

 $I_{x'} = I_x \cos^2 \theta - 2I_{xy} \sin \theta \cos \theta + I_y \sin^2 \theta$

$$I_{x'} = \int (y')^2 dA = \int (y \cos \theta - x \sin \theta)^2 dA$$
$$= \cos^2 \theta \int y^2 dA - 2\sin \theta \cos \theta \int xy \, dA + \sin^2 \theta \int x^2 \, dA \implies$$

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Similarly:

$$I_{y'} = I_x \sin^2 \theta + 2I_{xy} \sin \theta \cos \theta + I_y \cos^2 \theta$$
$$I_{x'y'} = (I_x - I_y) \sin \theta \cos \theta + I_{xy} (\cos^2 \theta - \sin^2 \theta)$$

Recalling the trigonometric relations

$$\begin{aligned} \sin 2\theta &= 2\sin\theta\cos\theta & \cos 2\theta = \cos^2\theta - \sin^2\theta \\ \cos^2\theta &= \frac{1+\cos 2\theta}{2} & \sin^2\theta = \frac{1-\cos 2\theta}{2} \end{aligned}$$

• The change of axes yields

$$I_{x'} = \frac{I_x + I_y}{2} + \frac{I_x - I_y}{2} \cos 2\theta - I_{xy} \sin 2\theta$$

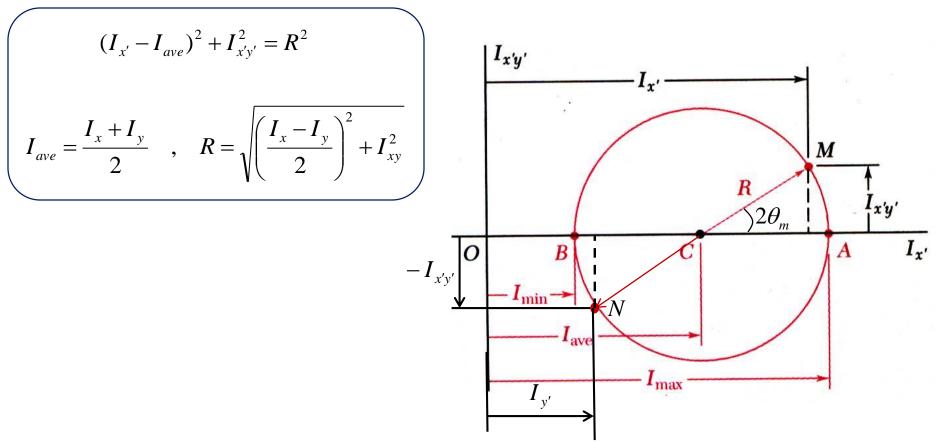
$$I_{y'} = \frac{I_x + I_y}{2} - \frac{I_x - I_y}{2} \cos 2\theta + I_{xy} \sin 2\theta$$

$$I_{x'y'} = \frac{I_x - I_y}{2} \sin 2\theta + I_{xy} \cos 2\theta$$
(1)

$$I_{x'} + I_{y'} = I_x + I_y$$

we eliminate θ from Eqs. (I)

• The equations for $I_{x'}$ and $I_{x'y'}$ are the parametric equations for a circle,



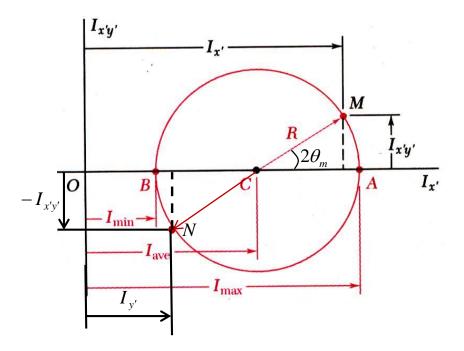
• At the points A and B, $I_{x'y'} = 0$ and $I_{x'}$ is a maximum and minimum, respectively.

$$I_{\max,\min} = I_{ave} \pm R \quad \Longrightarrow \quad$$

$$I_{\text{max, min}} = \frac{I_x + I_y}{2} \pm \sqrt{\left(\frac{I_x - I_y}{2}\right)^2 + I_{xy}^2}$$

$$\tan 2\theta_m = -\frac{2I_{xy}}{I_x - I_y}$$

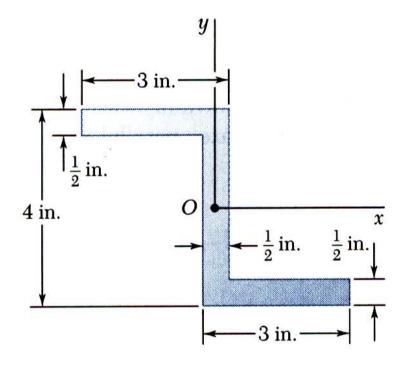
- The equation for θ_m defines two angles, 90° apart which correspond to the *principal axes* of the area about *O*.
- I_{max} and I_{min} are the principal moments of inertia of the area about O.



We note that if an area possesses an axis of symmetry through a point O, this axis must be a principal axis of the area about O. On the other hand, a principal axis does not need to be an axis of symmetry; weather or not an area possesses any axes of symmetry, it will have two principal axes of inertia about any point O.

For the section shown, the moments of inertia with respect to the x and y axes are $I_x = 10.38$ in⁴ and $I_y = 6.97$ in⁴.

Determine (a) the orientation of the principal axes of the section about O, and (b) the values of the principal moments of inertia about O.



SOLUTION:

• Compute the product of inertia with respect to the *xy* axes by dividing the section into three rectangles.

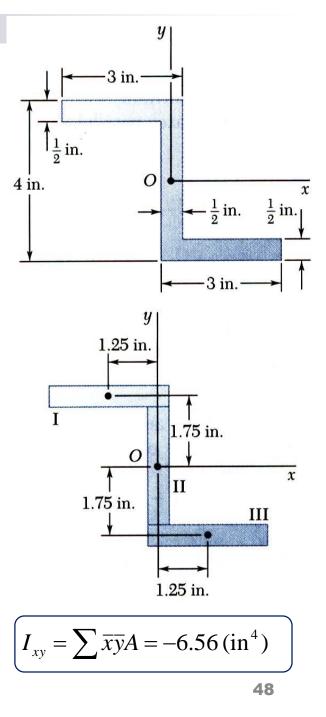
Apply the parallel axis theorem to each rectangle,

$$\left(I_{xy} = \sum (\bar{I}_{x'y'} + \bar{x}\bar{y}A)\right)$$

 $\bar{I}_{x'y'} = 0$

Note that the product of inertia with respect to centroidal axes parallel to the *xy* axes is zero for each rectangle.

Rectangle	Area, in ²	\overline{x} , in.	\overline{y} , in.	$\overline{x}\overline{y}A$, in ⁴
Ι	$3 \times \frac{1}{2} = 1.5$	-1.25	+1.75	-3.28
	$3 \times \frac{1}{2} = 1.5$			0
III	$3 \times \frac{1}{2} = 1.5$	+1.25	-1.75	-3.28
				$\sum \overline{x}\overline{y}A = -6.56$



SOLUTION:

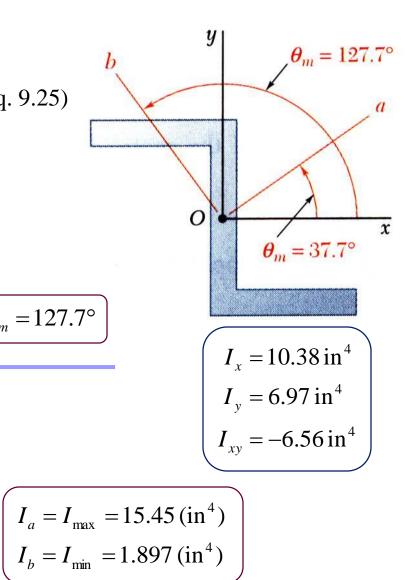
• Determine the orientation of the principal axes (Eq. 9.25) and the principal moments of inertia (Eq. 9. 27).

$$\tan 2\theta_m = -\frac{2I_{xy}}{I_x - I_y} = -\frac{2(-6.56)}{10.38 - 6.97} = +3.85$$

$$\Rightarrow 2\theta_m = 75.4^\circ \text{ and } 255.4^\circ$$

$$\Rightarrow \theta_m = 37.7^\circ, \ \theta_m = 127.7^\circ$$

$$I_{\text{max, min}} = \frac{I_x + I_y}{2} \pm \sqrt{\left(\frac{I_x - I_y}{2}\right)^2 + I_{xy}^2}$$
$$= \frac{10.38 + 6.97}{2} \pm \sqrt{\left(\frac{10.38 - 6.97}{2}\right)^2 + (-6.56)^2}$$

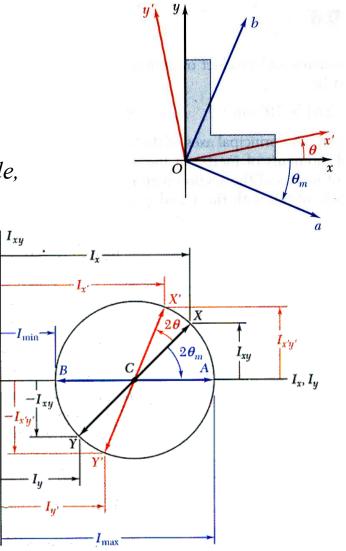


Mohr's Circle for Moments and Products of Inertia

Introduced by the German engineer **Otto Mohr** (1835-1918) and is known as **Mohr's circle**.

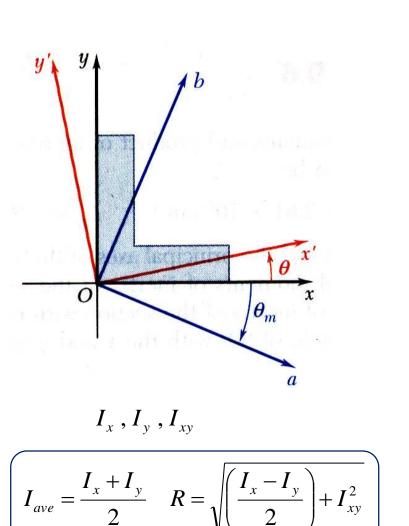
• The moments and product of inertia for an area are plotted as shown and used to construct *Mohr's circle*,

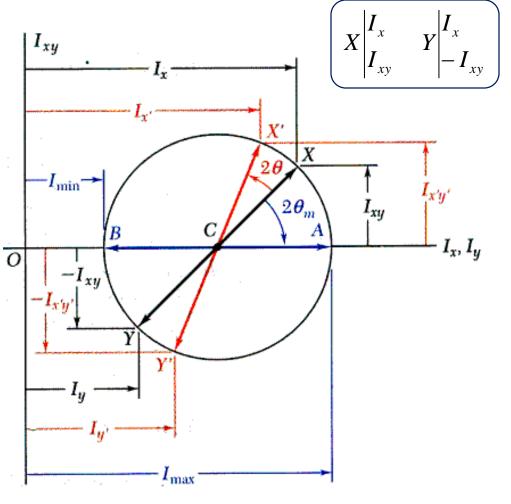
• Mohr's circle may be used to graphically or analytically determine the moments and product of inertia for any other rectangular axes including the principal axes and principal moments and products of inertia.



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Mohr's Circle for Moments and Products of Inertia

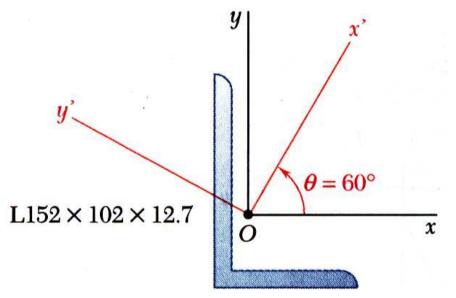




The moments and product of inertia with respect to the *x* and *y* axes are

$$I_x = 7.24 \times 10^6 \text{ mm}^4$$
, $I_y = 2.61 \times 10^6 \text{ mm}^4$, and $I_{xy} = -2.54 \times 10^6 \text{ mm}^4$.

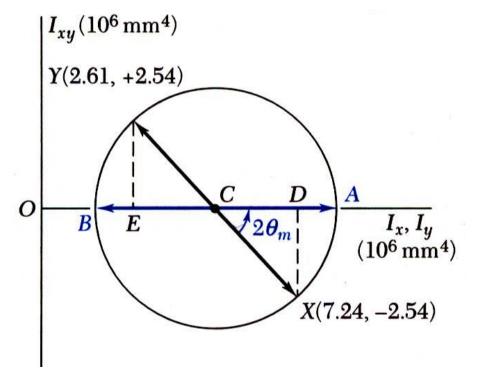
Using Mohr's circle, determine (a) the principal axes about O, (b) the values of the principal moments about O, and (c) the values of the moments and product of inertia about the x' and y' axes



SOLUTION:

 Plot the points (I_x, I_{xy}) and (I_y, -I_{xy}). Construct Mohr's circle based on the circle diameter between the points.

$$I_x = 7.24 \times 10^6 \text{ mm}^4$$
$$I_y = 2.61 \times 10^6 \text{ mm}^4$$
$$I_{xy} = -2.54 \times 10^6 \text{ mm}^4$$



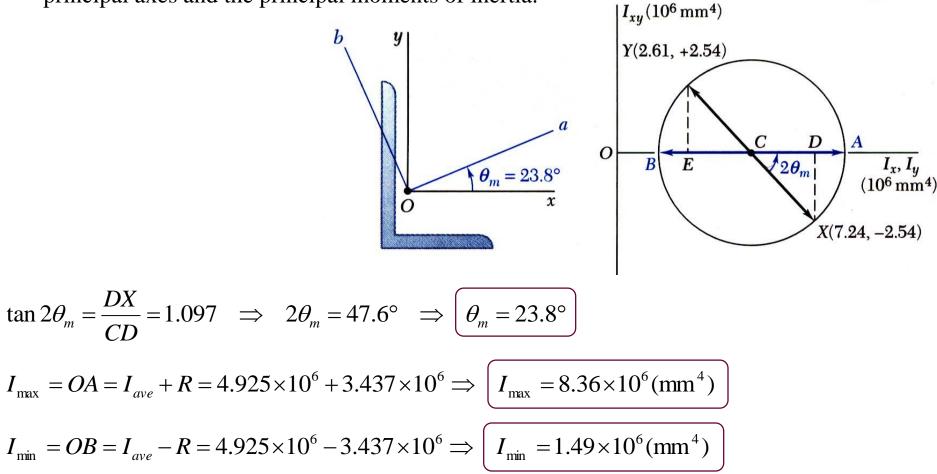
$$OC = I_{ave} = \frac{1}{2}(I_x + I_y) = \frac{1}{2}(7.24 \times 10^6 + 2.61 \times 10^6) \implies OC = 4.925 \times 10^6 (\text{mm}^4)$$

$$CD = \frac{1}{2}(I_x - I_y) = \frac{1}{2}(7.24 \times 10^6 - 2.61 \times 10^6) \implies CD = 2.315 \times 10^6 (\text{mm}^4)$$

$$R = \sqrt{(CD)^2 + (DX)^2} = \sqrt{(2.315 \times 10^6)^2 + (-2.54 \times 10^6)^2} \implies R = 3.437 \times 10^6 (\text{mm}^4)$$

SOLUTION:

• Based on the circle, determine the orientation of the principal axes and the principal moments of inertia.



SOLUTION:

The points X' and Y' corresponding to the x' and y' axes are obtained by rotating CX and CY counterclockwise through an angle $\theta = 2(60^\circ) = 120^\circ$. The angle that CX' forms with the x' axes is $\phi = 120^\circ - 47.6^\circ = 72.4^\circ$.

$$I_{x'} = OF = OC + CX' \cos \varphi = I_{ave} + R \cos 72.4^{\circ}$$

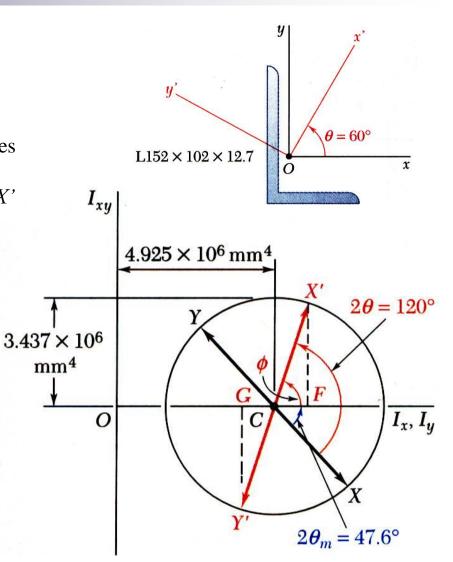
= 4.925×10⁶ + (3.437×10⁶) cos 72.4°
$$\Rightarrow I_{x'} = 5.96 \times 10^{6} (\text{mm}^{4})$$

$$I_{y'} = OG = OC - CY' \cos \varphi = I_{ave} - R \cos 72.4^{\circ}$$

= 4.925×10⁶ - (3.437×10⁶) cos 72.4^o
$$\Rightarrow I_{y'} = 3.89 \times 10^{6} (\text{mm}^{4})$$

$$I_{x'y'} = FX' = CY' \sin \varphi = R \sin 72.4^{\circ} = (3.437 \times 10^{6}) \sin 72.4^{\circ}$$

$$\Rightarrow I_{x'y'} = 3.28 \times 10^{6} (\text{mm}^{4})$$



$$OC = I_{ave} = 4.925 \times 10^{6} \,\mathrm{mm}^{4}$$
$$R = 3.437 \times 10^{6} \,\mathrm{mm}^{4}$$
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